

# DESY LINAC-III UPGRADE STUDY

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## Abstract

In the frame of the HERA luminosity upgrade program, the present performance of the HERA preinjectors has been studied in detail. Upgrading the proton linac (Linac III) energy from 50 MeV to 160 MeV is one possibility currently under discussion to obtain higher luminosity. Taking into account the limited space between the existing setup and the injection beam line to the DESY III, DESY's proton synchrotron, an upgrade study of an 810 MHz linac has been carried out. The results are summarized in this paper and some aspects are discussed leading to the solution presented here.

## Introduction

The present transport channel from Linac III to the synchrotron is long enough in order to use the straight beam line downstream of the last tank of the Drift Tube Linac (DTL) for installation of additional accelerating structures in order to upgrade the energy of the H<sup>-</sup> linac. According to our study a frequency of 810.24 MHz should be used for the upgraded part. Using four times the frequency of the 50 MeV Alvarez linac allows to obtain a high accelerating gradient which accelerates the H<sup>-</sup> beam up to 160 MeV over a distance of approximately 33 m. A higher injection energy could be a remedy against beam emittance blow-up in the DESY Synchrotron and finally would allow beams with higher brightness in HERA.

Using existing diagnostic equipment in the Linac, both the longitudinal and transverse emittances have been reconstructed by measuring the momentum spread and beam profiles [1,2,3]. In order to estimate the full emittance an elliptical symmetry for lines with constant density in phase space has been assumed. The final values of the measured emittances, which have been used for the design of the upgraded linac part as well as the main beam characteristics of the LINAC III are presented in the Table 1.

## 2 General Design

In the energy range to be considered which in this case is greater than 50 MeV no efficient accelerating structures other than DTL's existed so far. However recent studies carried out mainly at Los Alamos Laboratories resulted in the development of accelerating structures for intermediate energies of light ions between 20 to 100 MeV [4]. The structure is a combination of the Coupled Cell Structure

(CCS) and DTL - CCDTL. Careful studies of the beam dynamics show that even for the 50 MeV beam with the characteristics listed in Table 1, an operating frequency for a CCDTL four times higher as compared to the Linac III frequency is appropriate. The use of a 810 MHz structure allows to achieve a high accelerating gain. In addition 810 MHz klystrons are available (e.g. supplied by LITTON) as with small modifications as compared to the 805 MHz klystrons which have been developed for the Fermilab linac upgrade [5]. Also the modulator system could be very similar to the Fermilab design [5] except for the average power which is 30 times smaller.

Table 1: Linac III beam parameters

Repetition rate, Hz	1
Pulse length, $\mu$ s	30
Pulse current, mA	20
Energy, MeV	50
Emittance:	
Long. ( $\phi$ - $\phi_s$ , $\Delta W/W$ )	
$\alpha$	0.0
$\beta$ , deg./%	40.7
$\epsilon_{l,eff}$ , deg-%, rms	1.55
90%	4.48
~100%	9.68
Horizontal&Vertical	
$\alpha_x$	0.035
$\beta_x$ , mm/mrad	5.59
$\epsilon_x$ , $\pi$ -mm-mrad, rms	2.06
90%	9.6
~100%	33
$\alpha_y$	0.885
$\beta_y$ , mm/mrad	14.45
$\epsilon_y$ , $\pi$ -mm-mrad, rms	1.81
90%	4.1
~100%	29

Providing a high accelerating gradient and the use of the fourth harmonic on the other hand results in some disadvantages which must be taken into account:

- Smaller longitudinal acceptance with respect to the Linac III DTL;
- High accelerating gradient causes a coupling of longitudinal and transverse motion which produce transverse emittance growth.

Both transverse and longitudinal motions of the particles require a transition

region (TR) at the output of the present DTL. Using a 12 MW klystron the upgraded part of Linac must be divided into three parts. Each part is powered by a separate klystron. With one CCDTL part an energy gain of approximately 40 MeV can be achieved while the other two parts are based on a more conventional CCS. Considering in addition proper beam focusing results in 10 accelerating sections with constant phase velocity and 9 coupling bridges in the CCDTL part and 6 accelerating sections and 5 bridges in each CCS part. The quadrupole lenses are placed between the sections as well as the cavities to provide a FODO lattice. The design of the CCS has been made, taking into account that each accelerating section consists of 16 cells each.

Special attention has been given to the distance between the sections. It is obvious that this length must be as small as possible from the requirements determined by the

longitudinal beam motion. In practice this distance is chosen according to the design of the focusing lenses which are installed in between, as well as steering magnets and beam instrumentation required at these places. For linacs operating today which are based on the CCS, this space is an odd multiple of  $\beta\lambda/2$  and the shortest length of  $3\beta\lambda/2$  has been realized for example in the upgraded Fermilab linac. In the energy range between 50 to 100 MeV this value is not sufficient to fit the equipment mentioned before and we decided to choose the inter-section distance in the CCDTL cavity equal to  $2\beta\lambda$  while for the CCL this distance is  $3\beta\lambda/2$ . Rectangular coupling bridges operating in a  $TE_{11n}$  mode are planned for coupling of accelerating sections in each part. This type of bridge has been successfully applied in the main part of INR linac [6]. The  $TE_{11n}$  bridge avoids mode mixing, provide the space needed for equipment and can provide either  $\pi$  or  $2\pi$  phase shift between accelerating sections.

### The Accelerating structure

The well known Side Coupled Structure (SCS) could be a good solution for the Linac Upgrade. However relatively large number of cells in the CCL sections (96) require strong coupling ( $> 5-7\%$ ), which is more than typically used for the SCS. The use of a SCS in the CCDTL would result in even smaller coupling ( $\sim 1\%$ ). On the other hand the Disk and Washer (DAW) structure can be used for this purpose. Nevertheless, for a comparatively short linac (272 accelerating gaps in total), the development and production cost for DAW structure is higher as compared to the CCSs. In addition a DAWDTL has not been studied in detail and preliminary studies show that more interfering modes exist. Methods to remove parasitic modes from the vicinity of the operating mode, which have been developed for standard DAW structures, are not evidently effective in DAWDTL and need more detailed analysis.

An On-axis Coupled Structure (OCS) was chosen in order to provide a larger coupling constant. In addition this structure is comparatively simple from the mechanical point of view and with the low repetition rate (heat load of the structure is only 60 W/m) it is not necessary to use internal cooling of the accelerating cells. A sketch of the OCS and OCSDTL is shown in Figure 1 and 2.

An OCS has been used already in many electron machines. For the upgrade we have studied and optimized the On-axis Coupled Structure for cells, which are used in the velocity range of  $0.3 < \beta < 0.52$ , with the 2D/3D MAFIA code [7].

A few key points have been taken into account:

- The maximum surface field is 1.35 of Kilpatrick limit ( $36.2 \text{ MV/m} = 1.35 \times 26.1 \text{ MV/m}$ ).
- The shape of the accelerating cells has been optimised using a 2D approximation, both for OCS and OCSDTL option.

- To reduce possible sparking rate during transients in the coupling cells the ratio of  $E_{c,max} / \sqrt{W_c}$  has been limited. Here  $E_{c,max}$  is a maximal electric field on the surface for the coupling mode for given value of the energy  $W_c$  stored in a coupling cell.

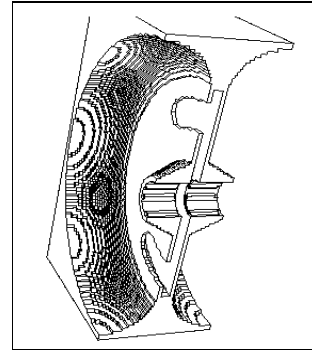


Fig. 1. The general view of the On-Axis Coupled Structure.

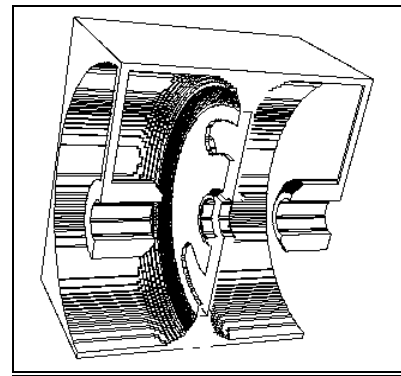


Fig. 2. The general view of the On-Axis Coupled Structure combined with the drift tubes.

- The coupling slots have been investigated and optimised. The axial length of the slot has been varied to achieve a coupling constant of 15% for OCS sections and 10% for OCSDTL sections.

The calculated values of  $ZT^2$ , taking some degradation into account and  $E_0T$  for the finally chosen option of the OCSDTL and OCS are plotted in Figure 3.

### Beam Dynamics

The accelerating structure geometry has been modeled using functions of the effective accelerating gradient  $E_0T$ , effective shunt resistance  $ZT^2$  and the gap ratio  $\alpha_g$  with respect to the relative beam velocity  $\beta$ , as being obtained from the MAFIA calculations. A general parameter list of the upgraded Linac is given in the Table 2.

Due to the different periodicity of the focusing structure in section 1 ( $16\beta\lambda$ ) and section 2 ( $19\beta\lambda$ ), matching of the transverse beam dimensions is necessary between these two sections. This is provided using four quadrupole lenses at the end of the cavity 1.

The main component of the transition region (TR) is a buncher cavity followed by a drift space in order to reduce the phase spread of the 202.56 MHz bunches from  $\pm 13^\circ$  to  $\pm 4^\circ$  as is required for the matching conditions at the entrance of the upgraded linac. The TR contains four quadrupoles to match the transverse phase space parameters.

In Figure 4 the beam envelopes (x-plane = solid line, y-plane = dashed line), the relative energy spread  $\Delta W/W$  and the phase spread  $\Delta\phi$  of 90% of the particles are presented along the longitudinal coordinate for the upgraded part of the linac. The simulation has been performed for all 100% particles including a beam halo. The beam losses are less than 0.04%. An rms-emittance growth of 22 % in the transverse phase planes due to the rf defocusing has been calculated.

Several sources of accelerator imperfections and their effect on beam dynamics have been studied. The conventional random deviation of linac parameters from the design values produce a transverse rms-emittance growth of 20 % and a longitudinal rms emittance growth of 3 % with a probability of 90%. Two other sources of accelerating field distortions in a long CCS cavity are:

- a natural drop of the rf power along the cavity containing a large number of coupled cells;
- transient beam loading and compensation schemes. The first effect is negligible due to the high cell coupling. The latter slightly increases the momentum spread of a 20 mA beam for a very short part of the beam pulse.

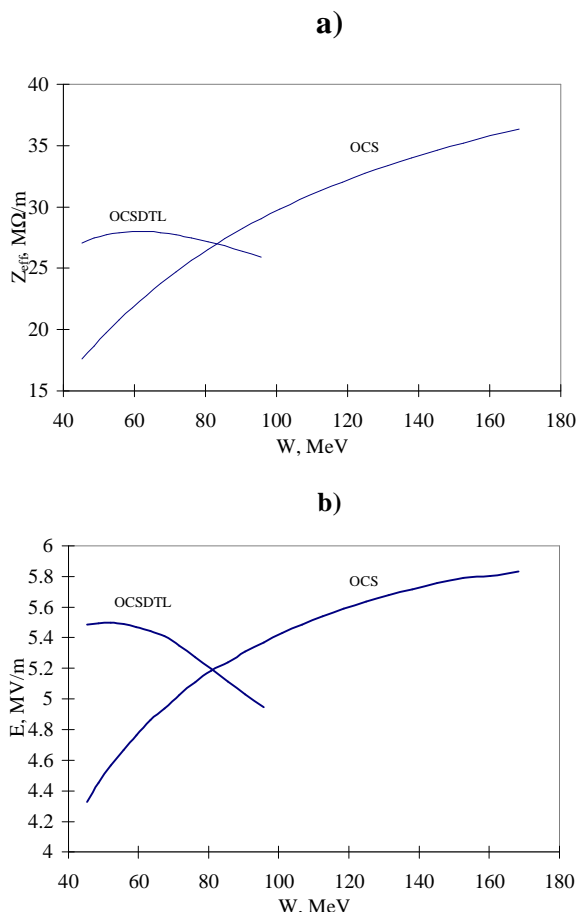


Fig. 3. Effective shunt impedance (a) and accelerating gradient (b) as a function of beam energy.

Table 2: General parameters of the upgraded linac

Parameter	Cavity 1	Cavity 2	Cavity 3
Initial kinetic energy, MeV	50	85.412	119.86
Final kinetic energy, MeV	85.412	119.86	159.75
Total length, m	10.630	9.112 m	10.084 m
Frequency, MHz	810.24	810.24	810.24
Synchronous phase	$-35^\circ$	$-35^\circ$	$-35^\circ$
Number of sections	10	6	6
Number of cells per section	4	16	16
Type of structure	OCSDTL	OCS	OCS
Focusing structure	FODO	FODO	FODO
Section separation $\beta\lambda$	2	3/2	3/2
Section length $\beta\lambda$	6	8	8
Length of focus. period $\beta\lambda$	16	19	19
Cavity bore radius, cm	1.5	1.5	1.5
Power consumption, MW	9	8.5	9.0 MW
copper loss, MW	8.288	7.816	8.196
beam power, MW	0.708	0.689	0.798

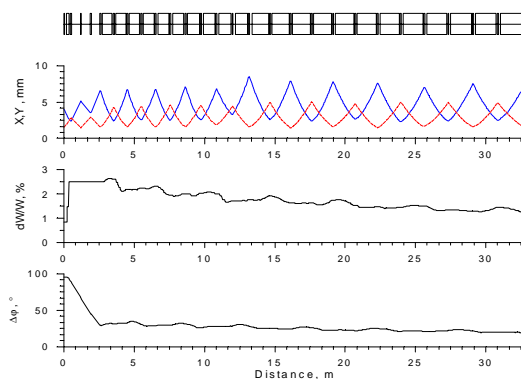


Fig. 4. Beam envelopes (90% of particles) along the linac.

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